

IN THE SPECIFICATION

Please amend paragraph 1 as follows:

This patent application claims priority from U.S. Provisional Patent Application serial number 60/453,316 filed on March 10, 2003 and from U.S. Provisional Patent Application serial number 60/464,917 filed on April 23, 2003. This patent application is a continuation in part of U.S. Patent 6,609,568 issued on August 26, 2003 Application no. 09/910,209, entitled Closed-Loop Draw down Apparatus and Method for In-Situ Analysis of Formation Fluids, by V. Krueger et al. filed on July 20, 2001, published on August 22, 2002 which is incorporated herein by reference in its entirety, hereinafter referred to as "the Krueger application", which along with the current application is commonly owned by Baker Hughes, Incorporated Inc.

Please amend paragraph 10 as follows:

[0010] The parent application for the present invention, U.S. Patent number 6,609,568 teaches the Krueger application provides a formation rate analysis (FRA) apparatus and method that addresses some of the drawbacks described above by utilizing a closed-loop apparatus and method to perform formation pressure and permeability tests more quickly than the devices and methods described above. With quicker formation testing, more tests providing actual pressures and permeability may be provided to enhance well operation efficiency and safety. U.S. Patent number 6,609,568 The Krueger application provides an apparatus and method capable of creating a test volume within a borehole, and incrementally decreasing the pressure within the test volume at a variable rate to allow periodic measurements of pressure as the test volume pressure decreases. Adjustments to the rate of decrease are made before the pressure stabilizes thereby eliminating the need for multiple

cycles. This incremental draw down apparatus and method will significantly reduce overall measurement time, thereby increasing drilling efficiency and safety.

Please amend paragraph 14 as follows:

[0014] The novel features of this invention, as well as the invention itself, will be best understood from the attached drawings, taken along with the following description, in which similar reference characters refer to similar parts, and in which:

Fig. 1 is a graphical qualitative representation a formation pressure test using a particular prior art method;

Fig. 2 is an elevation view of an offshore drilling system according to one embodiment of the present invention;

Fig. 3 shows a portion of drill string incorporating the present invention;

Fig. 4 is a system schematic of the present invention;

Fig. 5 is an elevation view of a wireline embodiment according to the present invention;

Fig. 6 is a plot graph of pressure vs. time and pump volume showing predicted drawdown behavior using specific parameters for calculation;

Fig. 7 is a plot graph of pressure vs. time showing the early portion of a pressure buildup curve for a moderately low permeability formation;

Fig. 8 is a plot graph of a method using iterative guesses for determining formation pressure;

Fig. 9 is a plot graph of a method for finding formation pressure using incomplete pressure buildup data;

Fig. 10 is a plot graph of pressure vs. draw rate illustrating a computation technique used in a method according to the present invention to determine formation pressure;

Fig. 11 is a graphical representation illustrating a method according to the present invention;

Fig. 12 is an illustration of a wire line formation sampling tool deployed in a well bore;

Fig. 13 is an illustration of a bi-directional formation fluid pump for pumping formation fluid into the well bore during pumping to free the sample of filtrate and pumping formation fluid into a sample tank after sample clean up;

Fig. 14 of formation rate analysis data values for three strokes of the formation fluid pump;

Fig. 15 is a plot of formation fluid pump pressure, packer pressure, linear volume displacement of the pumping piston and pumping volume for three strokes of the sampling pump in a first example of problem free pumping of formation fluid;

Fig. 16 is a plot of pump pressure versus formation flow rate for the three strokes illustrated in Fig. 14 and Fig. 15. Note that the correlation coefficient (R^2) in Fig. 16 and Fig. 14 are above .99 indicating that the pumping speed is well matched to the formation flow rate;

Fig. 17 is a second example of pumping history showing a plot of formation fluid pump pressure, packer pressure, linear volume displacement of the pumping piston and pumping volume for three strokes of the sampling pump in a second example of pumping of formation fluid where a problem is apparent;

Fig. 18 is a plot for pressure versus formation rate for all pump strokes of the example of **Fig. 17** showing a correlation coefficient (R^2) of only 0.052, indicative of a problem; and

Fig. 19 is a plot for pressure versus formation rate for the first two pump strokes of the example of **Fig. 17** showing a correlation coefficient (R^2) of 0.9323, indicative of a quality sample up to that point; and

Fig. 20 is an illustration of a sampling tool where by a quality sample is pumped from a formation while measuring mobility/permeability versus time to ensure a single phase sample with low filtrate contamination, the sample having the same physical characteristics as it did when the sample existed in a formation.

Please amend paragraph 18 as follows:

[0018] In one embodiment of the present invention an extendable pad-sealing element 302 for engaging the well wall 4 (Fig. 1) is disposed between the packers 304 and 306 on the test apparatus 216. The pad-sealing element 302 could be used without the packers 304 and 306, because a sufficient seal with the well wall can be maintained with the pad 302 alone. If packers 304 and 306 are not used, a counterforce is required provided so pad 302 can maintain sealing engagement with the wall of the borehole 204. The seal creates a test volume at the pad seal and extending only within the tool to the pump rather than also using the volume between packer elements.

Please amend paragraph 33 as follows:

[0033] Pressure in the probe can be related to time by calculating the system volume as a function of time from Eq. 2. Conversely, if compressibility is not constant, its average value between any two system volumes is:

$$C_{avg} = \frac{\ln \left[\frac{V_{sys_{n+1}}}{V_{sys_n}} \right]}{P_2 - P_1} \quad (6)$$

where subscripts 1 and 2 are not restricted to being consecutive pairs of readings. Note that if temperature decreases during the drawdown, the apparent compressibility will be too low. A sudden increase in compressibility may indicate a pumping problem such as sanding, the evolution of gas or a leak past the packer on the seal between the probe face and the bore hole wall. The calculation of compressibility, under any circumstances, is invalid whenever pressure in the probe is less than formation pressure when fluid can flow into the probe giving the appearance of a marked increase in compressibility. Note, however, that compressibility of real fluids almost invariably increases slightly with decreasing pressure.

Please amend paragraph 69 as follows:

[0069] As illustrated in the partial sectional and schematic view of FIG. 13, the formation testing instrument 13 of FIG. 12 is shown to incorporate therein a bi-directional piston pump mechanism shown generally at 24 which is illustrated schematically in Fig. 13. Within the instrument body 13 is also provided at least one and preferably a pair of sample tanks which are shown generally at 26 and 28 and which may be of identical construction if

desired. The piston pump mechanism 24 defines a pair of opposed pumping chambers 62 and 64 which are disposed in fluid communication with the respective sample tanks via supply conduits 34 and 36. Discharge from the respective pump chambers to the supply conduit of a selected sample tank 26 or 28 is controlled by electrically energized three-way valves 27 and 29 or by any other suitable control valve arrangement enabling selective filling of the sample tanks. The respective pumping chambers are also shown to have the capability of fluid communication with the subsurface formation of interest via pump chamber supply passages 38 and 40 which are defined by the sample probe 18 of FIG. 12 and which are controlled by appropriate valving. The supply passages 38 and 40 may be provided with check valves 39 and 41 to permit overpressure of the fluid being pumped from the chambers 62 and 64 if desired. Position Sensor Resistor LMP 47 tracks the position and speed of pistons 58 and 60 from which pumping volume, over time, for a known piston cylinder size can be determined.

Please amend paragraph 91 as follows:

[0091] As shown in Fig. 14, mobility and compressibility changes for each pump stroke, but are very close. Mobility increases only slightly. The FRA for three pumping strokes as combined generates a de facto average of sorts over three pumping strokes for compressibility and mobility. Turning now to Fig. 16, the FRA plot 1604 for the three pumping strokes combined, as shown in Fig. 16 illustrates a relatively good correlation to a straight line 1602 of 0.9921. The above example indicates the FRA can be successfully applied to pumping data when the Reservation Characterization Instrument TM (RCI) 56 cc (BB) pump is used and pumping volume (PTV) curves are turned on. FRA is applied to each stroke or can be applied to several strokes together in order to save computation time.

Please amend paragraph 94 as follows:

[0094] The present invention selects a portion of total draw down pump strokes and builds FRA data based on the calculated draw down rate. With the pumping data, an analysis interval is selected based on the number of pump strokes instead of draw down rate. The present invention uses a variable number of strokes through out the pumping, choosing a small pump strokes at the beginning, e.g., two or three pump strokes, and progressively increasing the number of pump strokes up to a selectable fixed maximum strokes, e.g., 10 strokes, or in the present example, approximately 500 cc of pumped fluid.

Please amend paragraph 96 as follows:

[0096] As shown in Fig. 20, pump 2018 pumps formation fluid from formation 2010. The formation fluid from the formation 2010 is directed either to the borehole exit 2012 during sample cleanup or to single phase sample tank 2020 and captured as sample 2021 once it is determined that the formation sample is cleaned up. The present invention enables monitoring of compressibility, permeability and mobility versus time in real time to enable quality control of the sample so that the sample remains in the same state as it existed in the formation. Borehole fluid 2016 surrounds the tool 2001. Packer 2024 contacts formation 2010. Formation fluid enters the tool 2001 on suction side 2014 of pump 2018 and exits pressure side 2016. Valve A 2022 allows fluid to enter single phase tank 2020 sample vessel or chamber 2021. Valve B 2026 allows fluid to exit 2012 to the borehole. The bottom chamber 2028 of single phase tank 2020 is open to the borehole pressure.